



**INFILTRATION TESTING PROGRAM
181 TORONTO STREET SOUTH
UXBRIDGE, ONTARIO
L9P 1R1**

**REPORT NO.: 5555-21-HD
REPORT DATE: August 25, 2023
REVISION 01**

**PREPARED FOR:
MAN HOLDINGS LTD.
174 DINNICK CRESCENT
TORONTO, ONTARIO
M4N 1M3**

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1 Introduction

1.1 Project Background

Toronto Inspection Ltd. (TIL) was retained by Man Holdings Ltd. (the Client) to carry out an infiltration testing program to assess the preliminary design of the proposed Low Impact Development (LID) at 181 Toronto Street South in the Township of Uxbridge, Ontario (the “Site”).

The physical address of the Site is as follows:

181 Toronto Street South
Uxbridge, Ontario, L9P 1R1

The is owned by the Client. Relevant information of the Client is as follows.

174 Dinnick Crescent
Toronto, Ontario, M4N 1M3

Based on a review of the Conceptual Site Plan prepared by John G. Williams Ltd. Architect (JGW) dated February 23, 2022, the proposed development at the Site consists of two, 3-storey buildings area to the east. Each building is also understood to have a basement level which is assumed to extend to approximately 2.5 metres below ground surface (mbgs) (8 ft). The Site will connect to municipal water and wastewater services on Toronto Street South. The Conceptual Site Plan prepared by Counterpoint Engineering (2022) is provided in **Appendix A**.

1.2 Site Description

The Site is located immediately east of Toronto Street South, west of Fred Barnaud Way, and approximately 50 m south of the intersection of these two roads. The Site covers an area of approximately 0.515 ha and near rectangular in shape.

The Site is currently vacant and covered by grass, weeds, and scattered trees.

Land uses adjacent to the Site are residential. The Site slightly slopes from south to north.

The location of the Site is shown in **Figure 1**

1.3 Objectives of the Infiltration Testing Program

The objective for the field infiltration testing program was to estimate the saturated field hydraulic conductivity and a representative unfactored infiltration rate within the soil overburden at the invert depths of the proposed low impact development (LID) features.

1.4 Groundwater Levels

A summary of static water level measurements at six monitoring wells in 2021 near the proposed LID are presented in **Table 1-1** and **Table 1-2** in meters below ground surface (mbgs) and in meters above sea level (masl), respectively. The monitoring well locations are provided in **Figure 1**. The borehole logs are provided in **Appendix A**.

Based on the measured groundwater levels between October and July 2021, up to 1.16 m's variability in the groundwater levels within each well was observed. Groundwater varied from a low of 274.12 masl to a high of 276.27 masl. The closest monitoring well to both test pits, 21BH-8 (MW), had a high-water level reading of 274.97 masl.

Table 1-1 Summary of Water Levels (mbgs)

Well ID	Screen Interval	25-Oct-21	7-Jan-22	16-Mar-22	28-Apr-22	04-Jul-22	31-Aug-22
	(mbgs)	(mbgs)	(mbgs)	(mbgs)	(mbgs)	(mbgs)	(mbgs)
21BH-1 (MW)	2.70 – 5.75	2.92	2.85	2.80	2.72	2.98	3.16
21BH-4 (MW)	2.89 – 5.90	2.82	2.77	2.72	2.66	2.89	3.04
21BH-8 (MW)	2.95.- 6.00	2.54	2.53	2.48	2.42	3.27	2.71

1. Water levels are relative to existing ground surface.

Table 1-2 Summary of Water Levels (masl)

Well ID	Screen Interval	25-Oct-21	7-Jan-22	16-Mar-22	28-Apr-22	04-Jul-22	31-Aug-22
	(masl)	(masl)	(masl)	(masl)	(masl)	(masl)	(masl)
21BH-1(MW)	276.29 - 273.24	276.07	276.14	276.19	276.27	276.01	275.83
21BH-4(MW)	275.86 – 272.81	275.89	275.94	275.99	276.05	275.82	275.67
21BH-8(MW)	274.44 - 271.39	274.85	274.86	274.91	274.97	274.12	274.68

2 Testing Location and In-Situ Soil

In total, two (2) test pits (23TP-1 and 23TP-2) were dug by an excavator to document the subsoil conditions and to facilitate field infiltration testing. The locations of the test pit are identified in **Figure 1**.

Based on observations made in the field, the test pits exposed up to 1.42 metre below ground surface (mbgs). At 23TP-1, a dark brown topsoil layer with sand, some gravel, trace silt and rootlets were in contact with ground surface and extends up to 0.18 mbgs. Below the top soil, a fill/ reworked area that consists of brown silty sand layer with some debris such as asphalt and building material, trace gravel and rootlets, followed by a brown sand layer, compact, with some silt, trace gravel, and moist was observed at 1.12 mbgs. 23TP-1 was dug up to 1.42 mbgs, no seepage was observed.

At 23TP-2, a dark brown topsoil layer with sand, some gravel, trace silt and some rootlets and organics was in contact with the ground surface and extends to 0.17 mbgs. Below the top soil, a brown silty sand layer with trace gravel, rootlets, organics, and debris such as asphalt was encountered, followed by a brown sand layer, compact, with some silt, trace gravel, and moist was observed at 1.11 mbgs. 23TP-2 was dug up to 1.41 mbgs, no seepage was observed.

The detailed visual observations from the test pits are presented in **Table 2-1**.

Table 2-1 Test Pit Observations

Test ID	Depth of Investigation (mbgs)	Soil Conditions	Water Seepage Observations
23TP-1	1.42	0 – 0.18 m – topsoil, dark brown, some gravel, rootlets, moist 0.18 – 1.12 m – silty sand, brown, trace gravel, trace rootlets, some debris, trace rootlets, moist 1.12 – 1.42 – sand, compact, brown, some silt, trace gravel	No seepage observed
23TP-2	1.41	0 – 0.17 m – topsoil, dark brown, some gravel, rootlets, organics, moist 0.17 – 1.11 m – silty sand, trace gravel, trace rootlets, trace organics, moist 1.11 – 1.41 m – sand, compact, brown, some silt, trace gravel	No seepage observed

Notes:

3 Laboratory Grain Size Analysis

Grain size analyses for selected soil samples were completed in the laboratory using sieve and hydrometer methods. The purpose of completing the grain size analyses was to determine the particle size distribution of the soil samples collected.

Grain size analyses were conducted using samples from the bottom of each test pit location to assess the particle size distribution at the location of the in-situ infiltration testing. The grain size distribution curves are attached as **Appendix B**. A summary of the results from the analyses are provided in **Table 3-1**.

Table 3-1 Hazen Permeability Summary

Test ID	Test Depth (mbgs)	Soil Category	Hazen Permeability (cm/s)	Laboratory Infiltration Rate (mm/hr)
23TP-1	1.42	Sand	1.4×10^{-5}	94
23TP-2	1.41	Sand	3.3×10^{-5}	75

4 In-situ Infiltration Test

In-situ infiltration testing was carried out using a Guelph Permeameter in accordance with the equipment's operating instructions (Soilmoisture Equipment Corp., 2012)¹. 6 cm diameter holes were hand-augured at the bottom of each test pit location.

The infiltration test details are summarized in **Table 4-1**. The approximate infiltration test locations are shown on **Figure 1** and the field Guelph Permeameter data tables documenting stabilization of drawdown rates are provided in **Appendix C**.

¹ Soilmoisture Equipment Corp. 2012. 2800 Guelph Permeameter Operating Instructions dated December 2012

Table 4-1 Infiltration Test Summary

Test ID	Test Depth	Well Hole Soil Description	Water Column Height	Reservoir Used	Method
	(mbgs)		(cm)		
23TP-1	1.42	Sand, compact, brown, some silt, trace gravel	5 & 10	Combined	Average of Single Heads
23TP-2	1.41	Sand, compact, brown, some silt, trace gravel	5 & 10	Combined	Average of Single Heads

Notes:

5 Test Results

5.1 Soil Condition

Based on the field logging of soil samples, the native subsoil at the base of the proposed LID consists of a layer of sand, compact, brown, some silt, trace gravel, and moist.

5.2 Estimated Field Hydraulic Conductivity and Infiltration Rate

The field saturated hydraulic conductivity (Kfs) was calculated using the “Guelph Permeameter Calculator” prepared by Soilmoisture Equipment Corp (2012)².

To determine the corresponding soil infiltration rate, the Kfs must be converted to a rate of infiltration (T). The approximate relationship between Kfs and T is provided in the Toronto and Region Conservation Authority (TRCA) *Stormwater Management Criteria* (TRCA, 2012)³ to complete this conversion.

It should be noted that the estimated field infiltration rates are specific to the areas tested at the Site and at the point in time when the tests were conducted. Test results may therefore not be applicable to other areas of the Site where subsurface conditions are not consistent with those of the test locations.

A summary of the Kfs from the current investigation is presented in **Table 5-1**. The calculation sheets from the Guelph Permeameter Calculator and field data are included in **Appendix C**.

Table 5-1 Unfactored Infiltration Rate from In-situ Infiltration Testing

Test Pit Location	Depth	Soil Unit	Saturated Hydraulic Conductivity Kfs (cm/s)	Unfactored Infiltration Rate (mm/hr) *
	mbgs			
23TP-1	1.42	Sand	1.15×10^{-3}	89
23TP-2	1.41	Sand	2.97×10^{-4}	61

Notes:

- * Unfactored Infiltration Rate at tested depth.

² Soilmoisture Equipment Corp. 2012. 2800 Guelph Permeameter Operating Instructions dated December 2012

³ Toronto and Region Conversation Authority (TRCA). 2012. Stormwater Management Criteria August 2012 Version 1.0.

6 Summary and Recommendations

The native subsoil at the base of the LID is observed to be sand, compact, brown, some silt, trace gravel. Based on the grainsize analyses and in-situ infiltration testing completed, an unfactored infiltration rate of 61 mm/hr for the bottom of the LID features is recommended. It will be at the discretion of the civil engineer to select a factor of safety to apply to the unfactored infiltration rate calculated.

It should also be noted that the field infiltration rates are specific to the areas tested at the Site, at the point in time when the tests were conducted. Test results may therefore not be applicable to other areas of the Site where subsurface conditions are not consistent with those at the test locations.

We trust that the findings from this investigation will meet your needs. Should you have any questions or comments, please do not hesitate to contact the undersigned.

Yours truly,

Toronto Inspection Ltd.

Kevin Nankisore, B.Sc., G.I.T.
Environmental Scientist

Shan Goel, P. Eng
Team Lead





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FIGURES



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APPENDIX A

Borehole Logs

Date Drilled: 4/8/21

Auger Sample



Headspace Reading (ppm)



Drill Type: Track Mounted Drill Rig

SPT (N) Value



Natural Moisture



Datum: Geodetic

Dynamic Cone Test



Plastic and Liquid Limit



Shelby Tube



Unconfined Compression



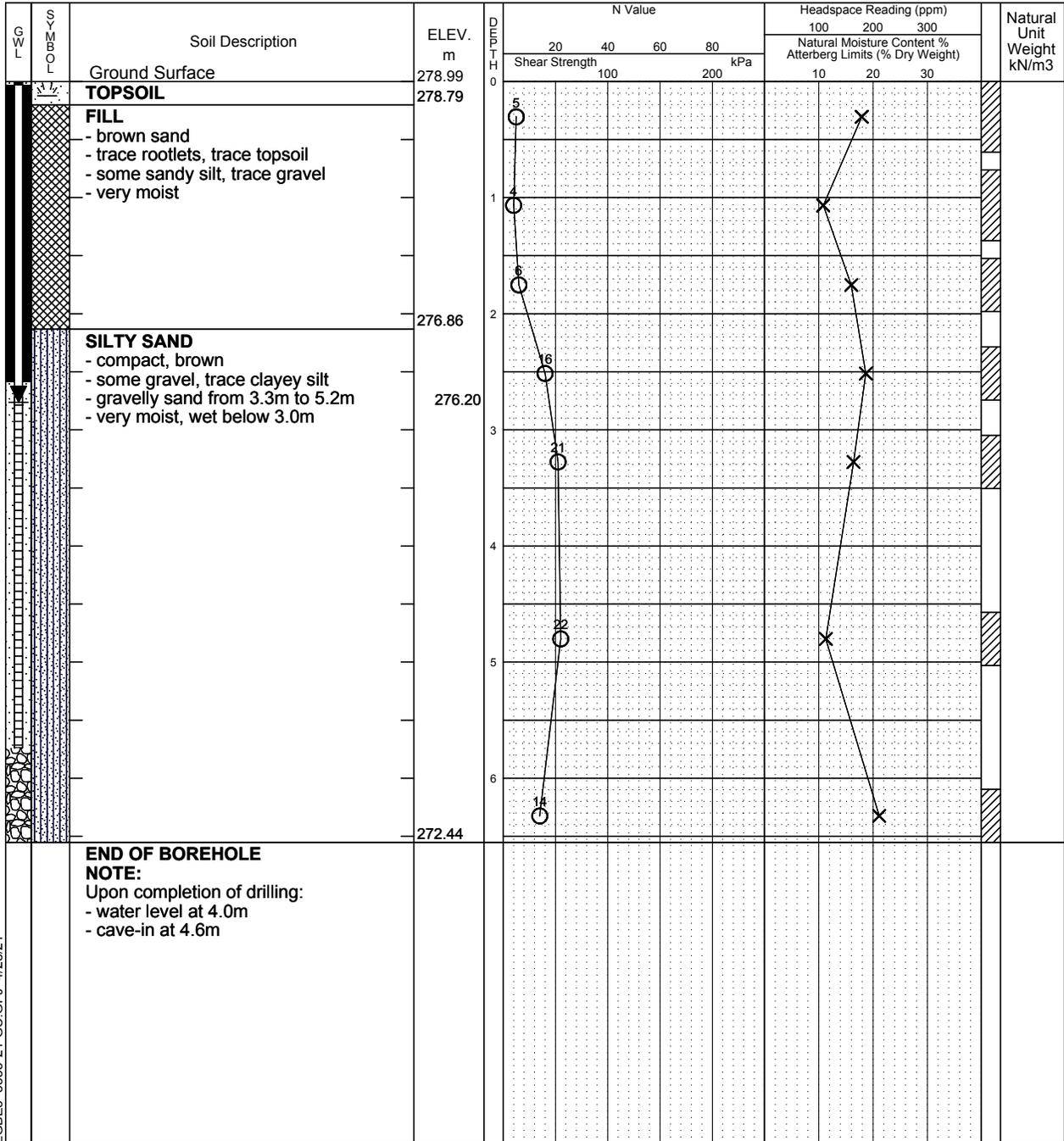
Field Vane Test



% Strain at Failure



Penetrometer



NOTE: THE BOREHOLE DATA NEEDS INTERPRETATION ASSISTANCE BY TORONTO INSPECTION LTD. BEFORE USE BY OTHERS

Toronto Inspection Ltd.

Time	Water Level (m)	Depth to Cave (m)
April 16, 2021	2.8m	

Date Drilled: 4/8/21

Auger Sample



Headspace Reading (ppm)



Drill Type: Track Mounted Drill Rig

SPT (N) Value



Natural Moisture



Datum: Geodetic

Dynamic Cone Test



Plastic and Liquid Limit



Shelby Tube



Unconfined Compression



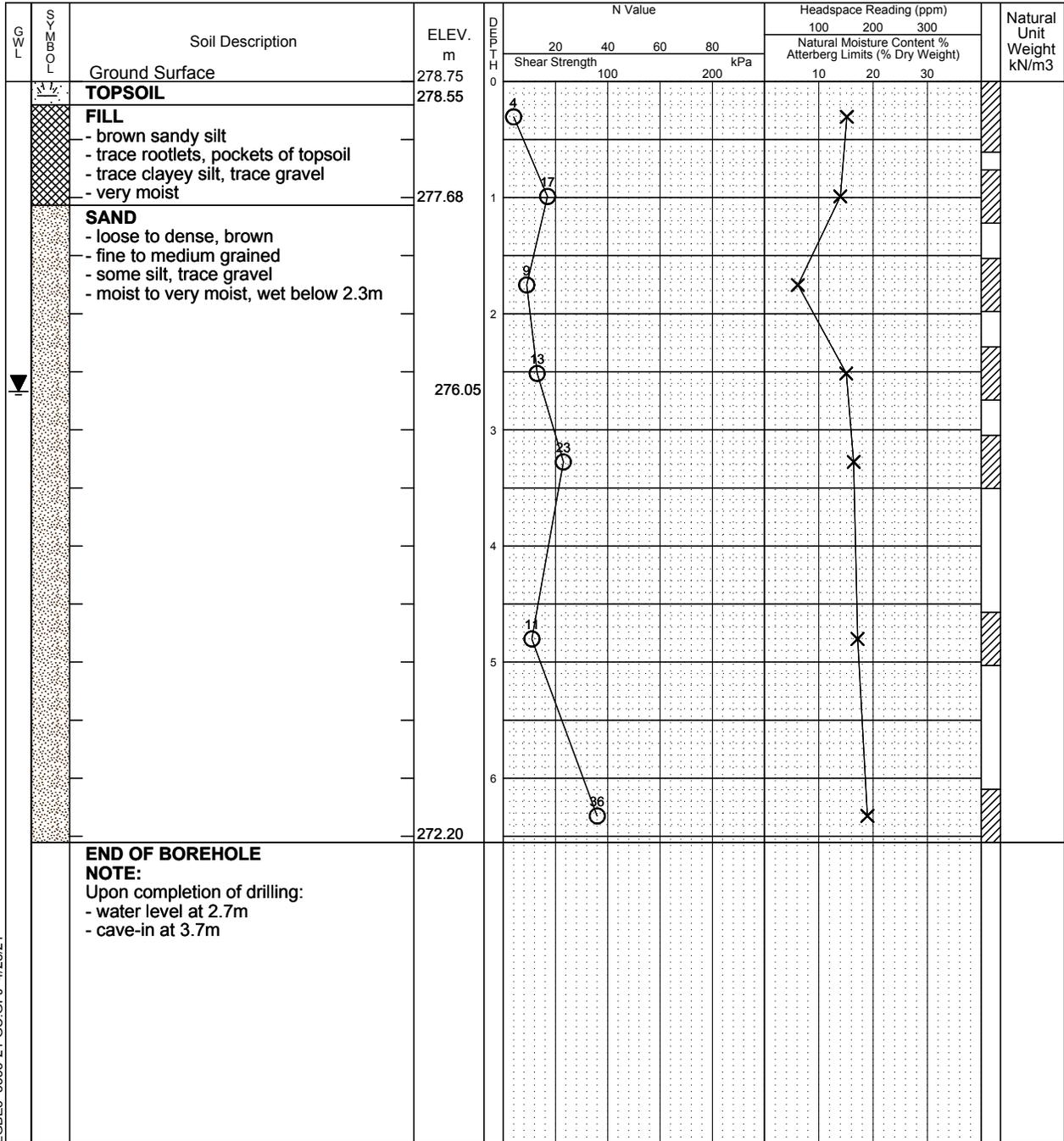
Field Vane Test



% Strain at Failure



Penetrometer



LGBE3 5555-21-GC.GPJ 4/28/21

NOTE: THE BOREHOLE DATA NEEDS INTERPRETATION ASSISTANCE BY TORONTO INSPECTION LTD. BEFORE USE BY OTHERS

Toronto Inspection Ltd.

Time	Water Level (m)	Depth to Cave (m)

Project: Geotechnical Investigation

Sheet No. 1 of 1

Location: 181 Toronto Street South, Uxbridge, Ontario

Date Drilled: 4/8/21

Auger Sample



Headspace Reading (ppm)



Drill Type: Track Mounted Drill Rig

SPT (N) Value



Natural Moisture



Datum: Geodetic

Dynamic Cone Test



Plastic and Liquid Limit



Shelby Tube



Unconfined Compression



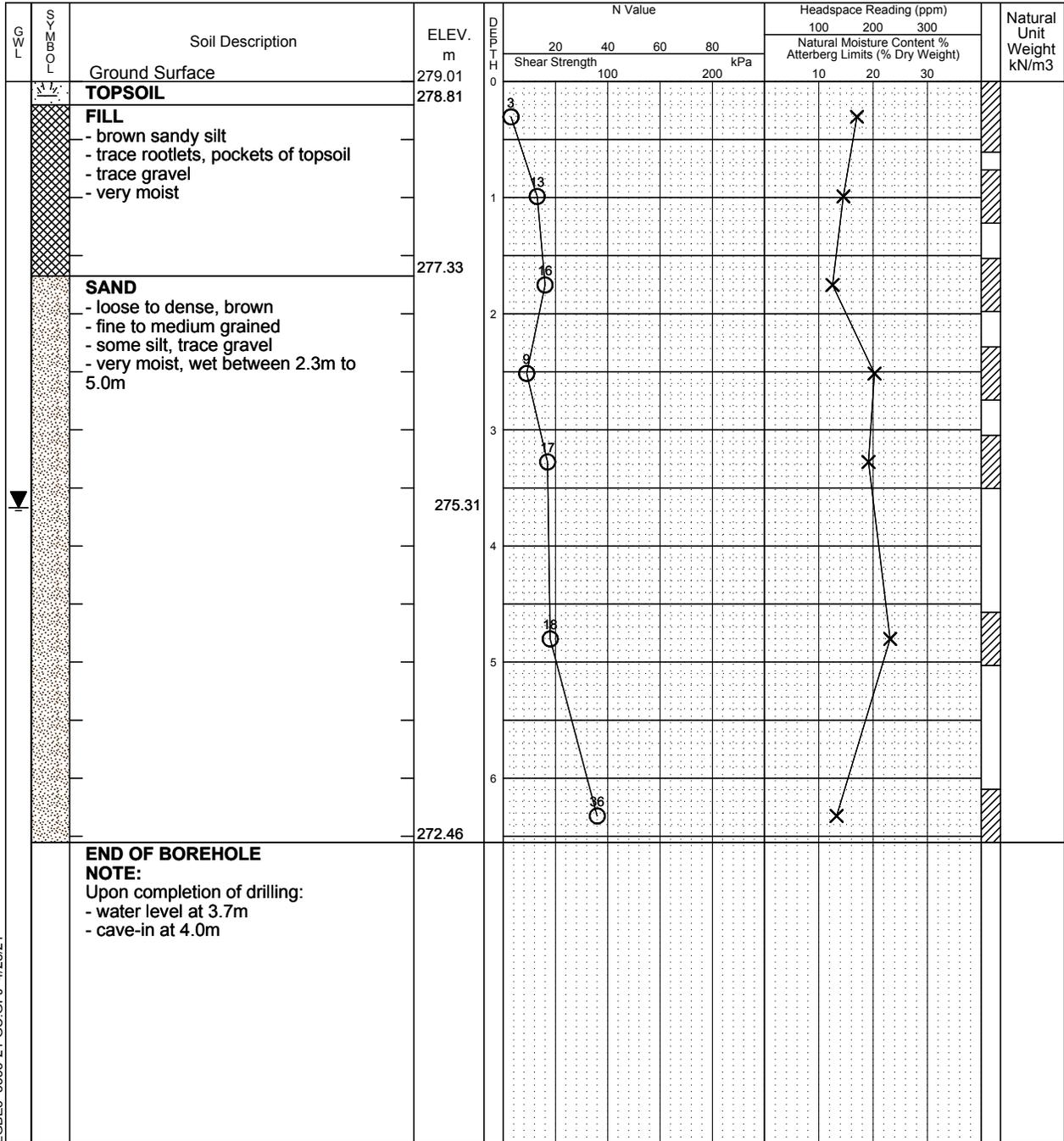
Field Vane Test



% Strain at Failure



Penetrometer



NOTE: THE BOREHOLE DATA NEEDS INTERPRETATION ASSISTANCE BY TORONTO INSPECTION LTD. BEFORE USE BY OTHERS

Toronto Inspection Ltd.

Time	Water Level (m)	Depth to Cave (m)

Date Drilled: 4/9/21

Auger Sample

Headspace Reading (ppm)

Drill Type: Track Mounted Drill Rig

SPT (N) Value

Natural Moisture

Datum: Geodetic

Dynamic Cone Test

Plastic and Liquid Limit

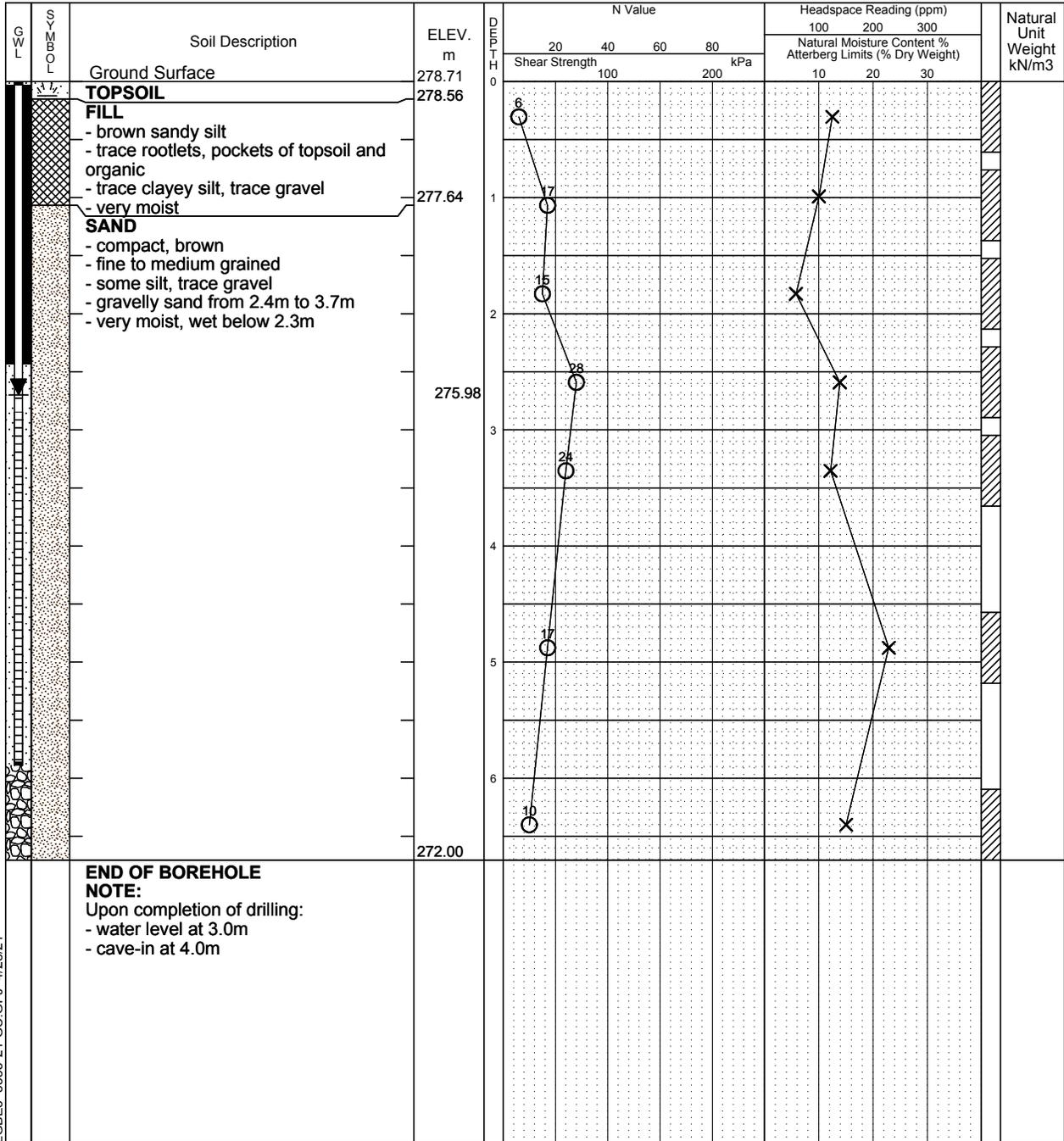
Shelby Tube

Unconfined Compression

Field Vane Test

% Strain at Failure

Penetrometer



NOTE: THE BOREHOLE DATA NEEDS INTERPRETATION ASSISTANCE BY TORONTO INSPECTION LTD. BEFORE USE BY OTHERS

Toronto Inspection Ltd.

Time	Water Level (m)	Depth to Cave (m)
April 16, 2021	2.7m	

Date Drilled: 4/8/21

Auger Sample



Headspace Reading (ppm)



Drill Type: Track Mounted Drill Rig

SPT (N) Value



Natural Moisture



Datum: Geodetic

Dynamic Cone Test



Plastic and Liquid Limit



Shelby Tube



Unconfined Compression



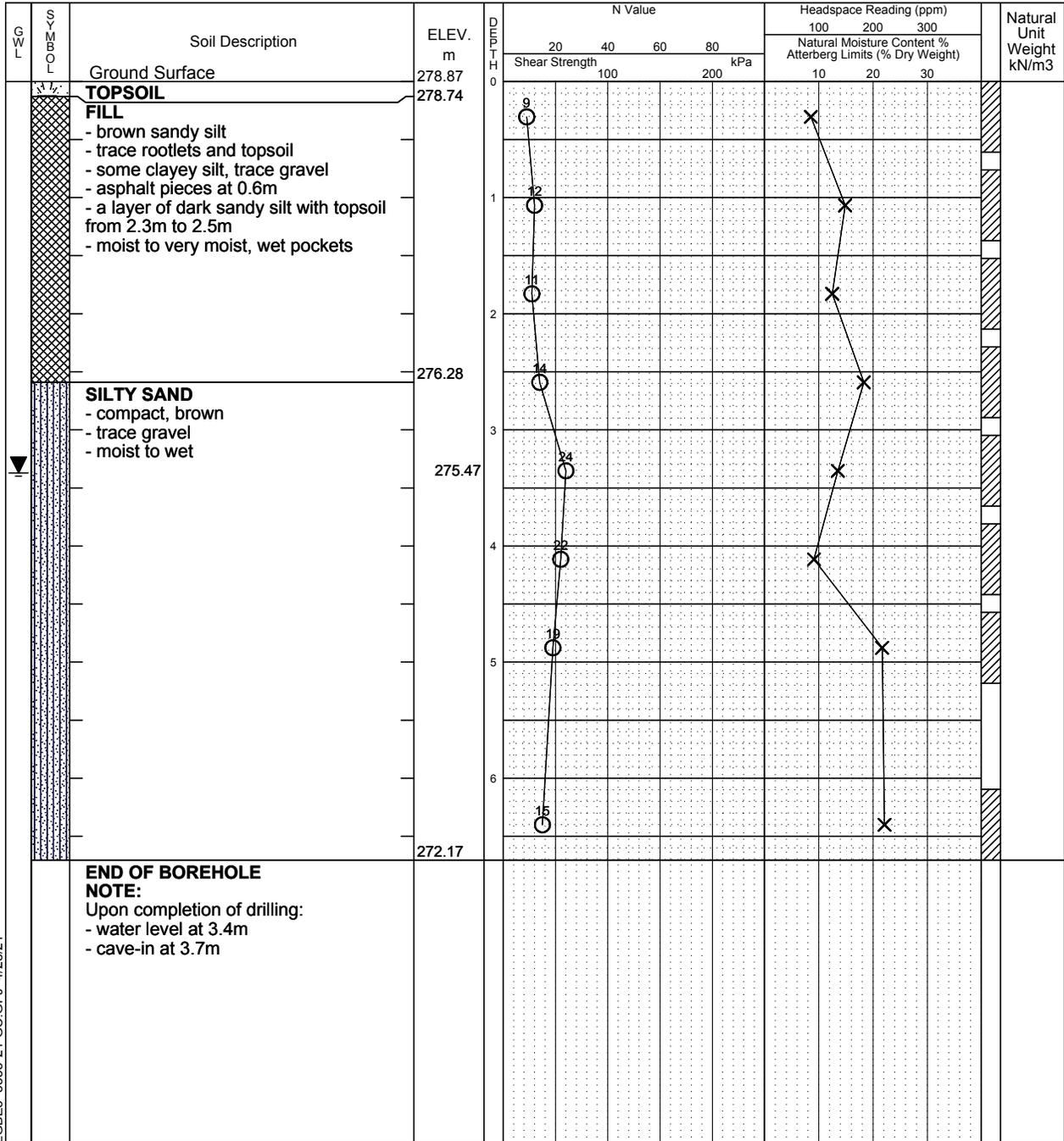
Field Vane Test



% Strain at Failure



Penetrometer



LGBE3 5555-21-GC.GPJ 4/28/21

NOTE: THE BOREHOLE DATA NEEDS INTERPRETATION ASSISTANCE BY TORONTO INSPECTION LTD. BEFORE USE BY OTHERS

Toronto Inspection Ltd.

Time	Water Level (m)	Depth to Cave (m)

Date Drilled: 4/9/21

Auger Sample



Headspace Reading (ppm)



Drill Type: Track Mounted Drill Rig

SPT (N) Value



Natural Moisture



Datum: Geodetic

Dynamic Cone Test



Plastic and Liquid Limit



Shelby Tube



Unconfined Compression



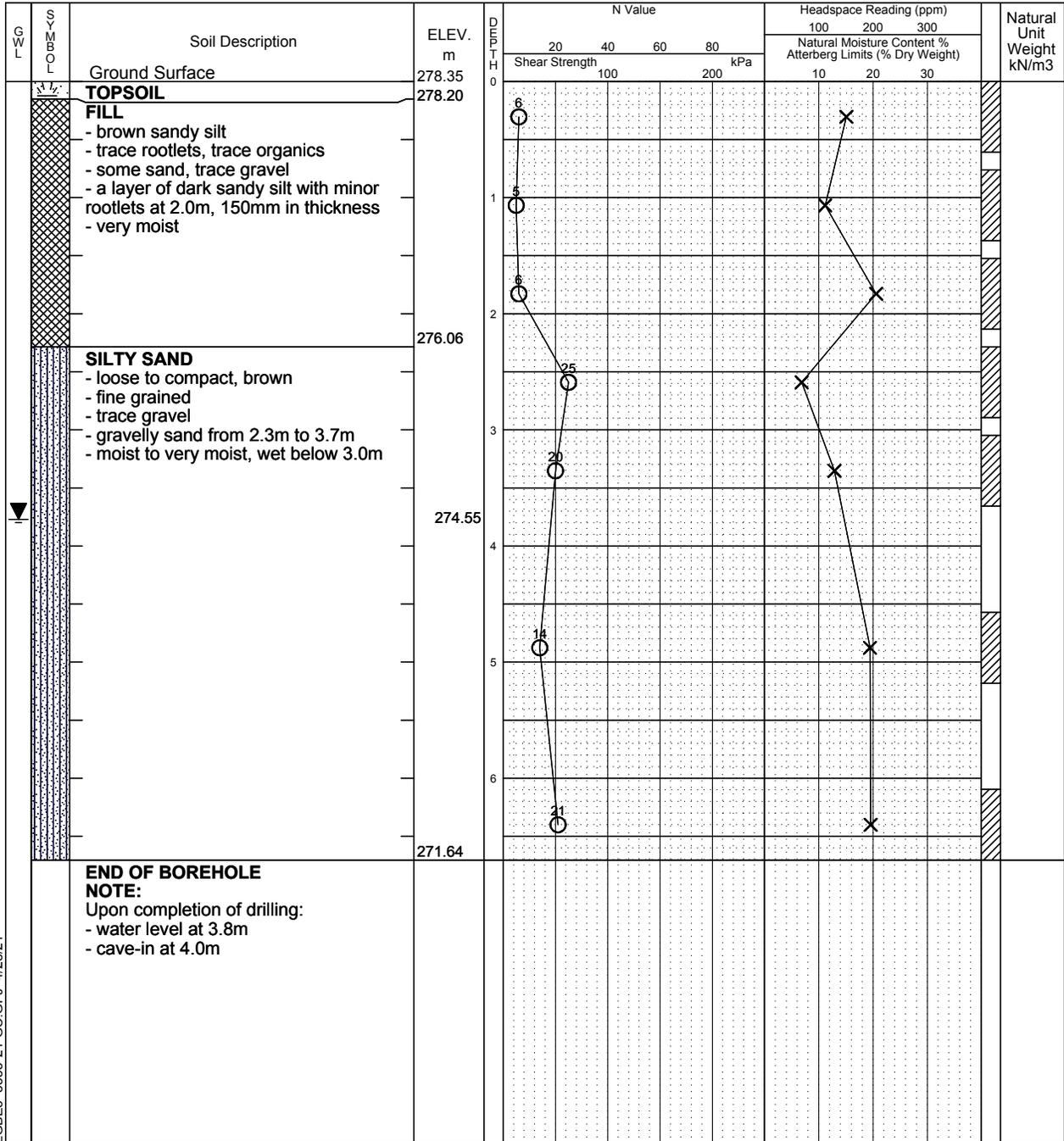
Field Vane Test



% Strain at Failure



Penetrometer



NOTE: THE BOREHOLE DATA NEEDS INTERPRETATION ASSISTANCE BY TORONTO INSPECTION LTD. BEFORE USE BY OTHERS

Toronto Inspection Ltd.

Time	Water Level (m)	Depth to Cave (m)

Date Drilled: 4/8/21

Auger Sample



Headspace Reading (ppm)



Drill Type: Track Mounted Drill Rig

SPT (N) Value



Natural Moisture



Datum: Geodetic

Dynamic Cone Test



Plastic and Liquid Limit



Shelby Tube



Unconfined Compression



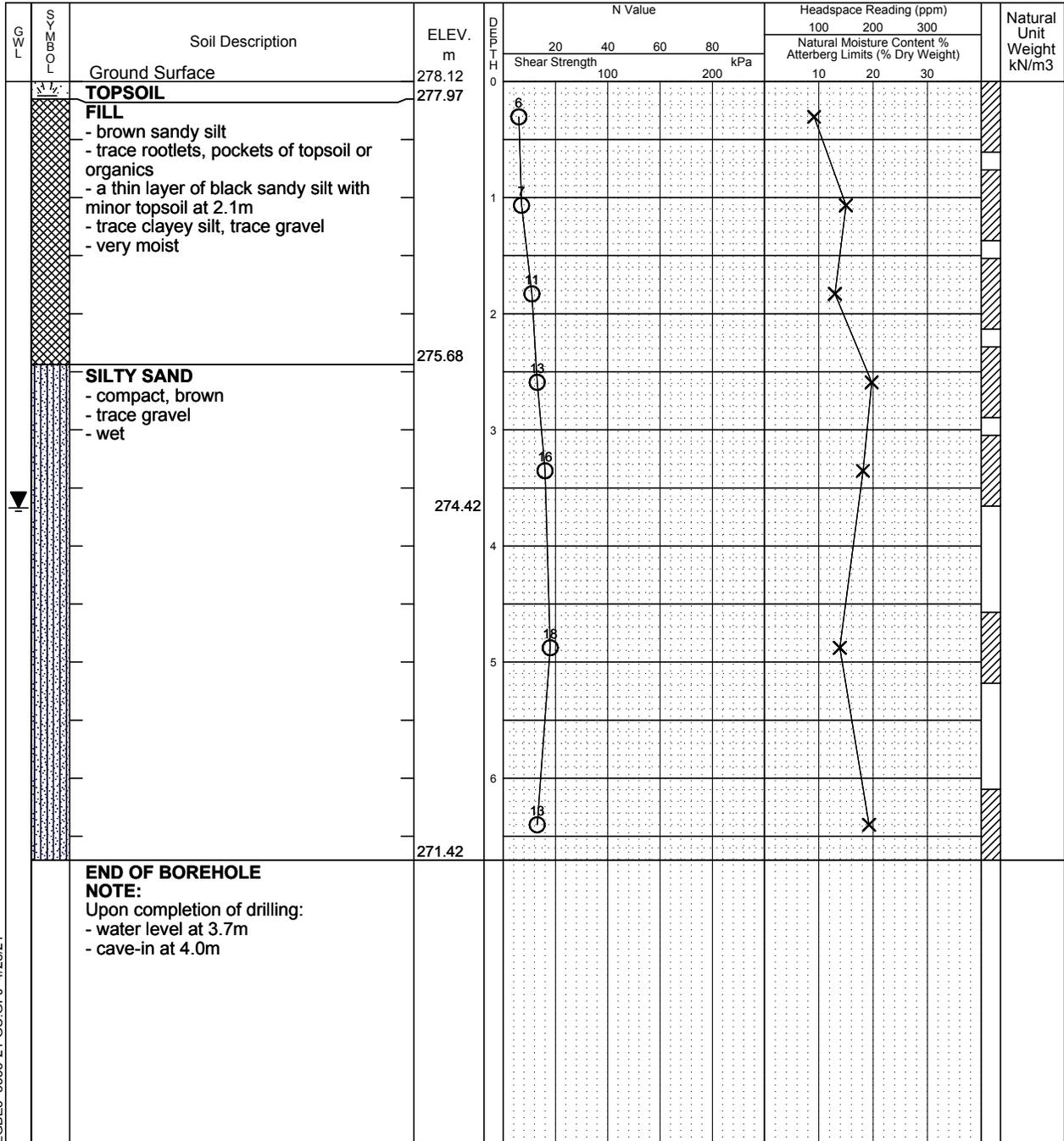
Field Vane Test



% Strain at Failure



Penetrometer



LGBE3 5555-21-GC.GPJ 4/28/21

NOTE: THE BOREHOLE DATA NEEDS INTERPRETATION ASSISTANCE BY TORONTO INSPECTION LTD. BEFORE USE BY OTHERS

Toronto Inspection Ltd.

Time	Water Level (m)	Depth to Cave (m)

Date Drilled: 4/8/21

Auger Sample



Headspace Reading (ppm)



Drill Type: Track Mounted Drill Rig

SPT (N) Value



Natural Moisture



Datum: Geodetic

Dynamic Cone Test



Plastic and Liquid Limit



Shelby Tube



Unconfined Compression



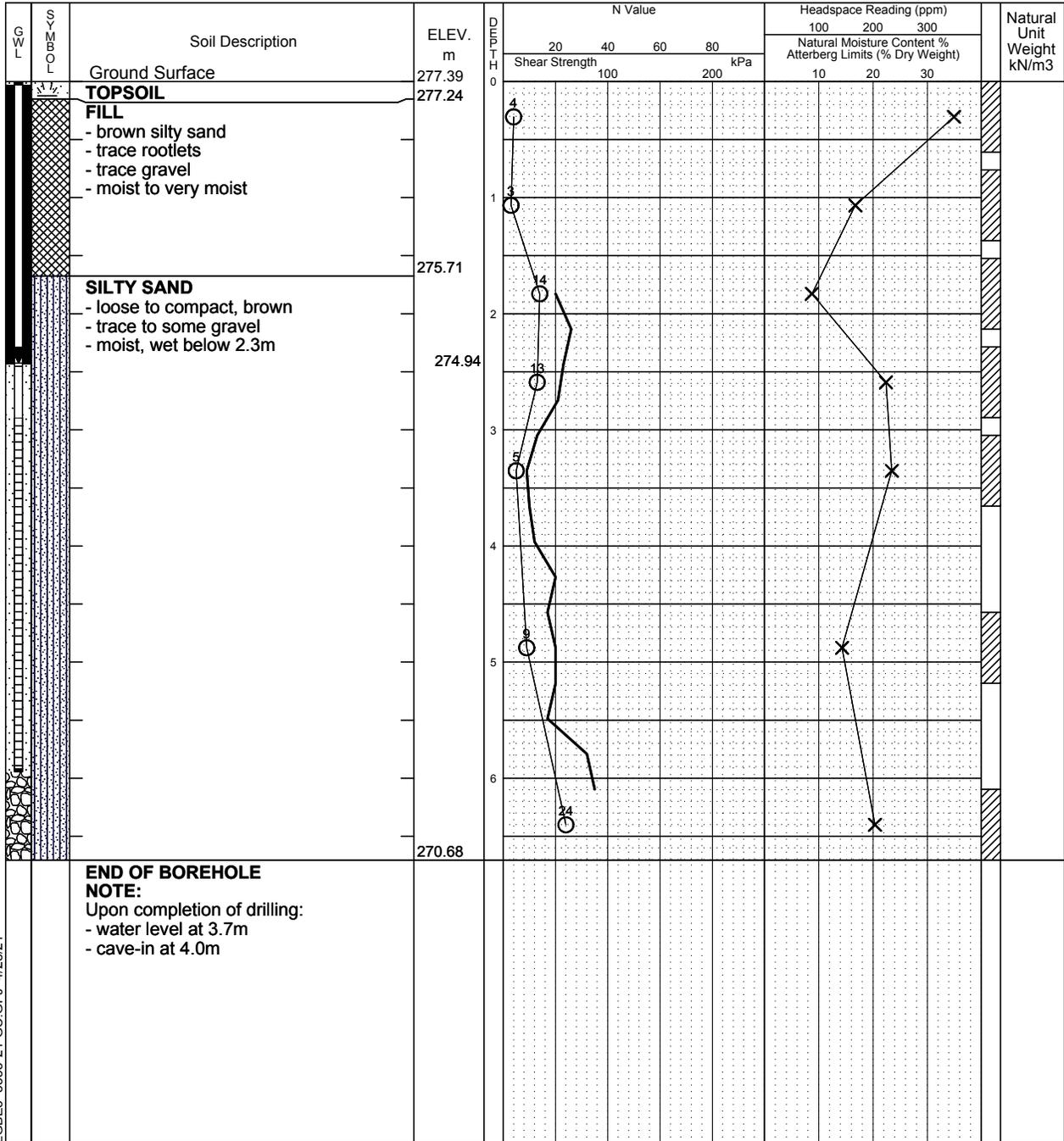
Field Vane Test



% Strain at Failure



Penetrometer



NOTE: THE BOREHOLE DATA NEEDS INTERPRETATION ASSISTANCE BY TORONTO INSPECTION LTD. BEFORE USE BY OTHERS

Toronto Inspection Ltd.

Time	Water Level (m)	Depth to Cave (m)
April 16, 2021	2.4m	

Project No. 5555-21-GC

Log of Borehole 21P-1

Dwg No. 10

Project: Geotechnical Investigation

Sheet No. 1 of 1

Location: 181 Toronto Street South, Uxbridge, Ontario

Date Drilled: 4/9/21

Auger Sample

Headspace Reading (ppm) ●

SPT (N) Value ○

Natural Moisture X

Dynamic Cone Test

Plastic and Liquid Limit

Shelby Tube

Unconfined Compression

Field Vane Test

% Strain at Failure

Penetrometer ▲

Drill Type: Track Mounted Drill Rig

Datum: Geodetic

G W L	SOIL LOG	Soil Description	ELEV. m	D I P T H m	N Value				Headspace Reading (ppm)			Natural Unit Weight kN/m ³		
					20	40	60	80	100	200	300		Natural Moisture Content % Atterberg Limits (% Dry Weight)	
					Shear Strength kPa				10	20	30			
		Ground Surface NO SAMPLING	278.54	0										
			277.32	1										
		SAND - loose, brown - fine to medium grained - gravelly - trace silt - moist END OF BOREHOLE NOTE: Upon completion of drilling:	276.87	5					X					

LGBE3 5555-21-GC.GPJ 4/28/21

NOTE: THE BOREHOLE DATA NEEDS INTERPRETATION ASSISTANCE BY TORONTO INSPECTION LTD. BEFORE USE BY OTHERS

Toronto Inspection Ltd.

Time	Water Level (m)	Depth to Cave (m)

Project No. 5555-21-GC

Log of Borehole 21P-2

Dwg No. 11

Project: Geotechnical Investigation

Sheet No. 1 of 1

Location: 181 Toronto Street South, Uxbridge, Ontario

Date Drilled: 4/8/21

Auger Sample



Headspace Reading (ppm)



Drill Type: Track Mounted Drill Rig

SPT (N) Value



Natural Moisture



Datum: Geodetic

Dynamic Cone Test



Plastic and Liquid Limit



Shelby Tube



Unconfined Compression



Field Vane Test



% Strain at Failure



Penetrometer



G W L	SOIL LOG	Soil Description	ELEV. m	D E P T H m	N Value				Headspace Reading (ppm)			Natural Unit Weight kN/m ³	
					Shear Strength kPa				Natural Moisture Content % Atterberg Limits (% Dry Weight)				
					20	40	60	80	100	200	300		10
		Ground Surface NO SAMPLING	277.72	0									
			275.89	1									
		SAND - dense, brown - some gravel, some silt - moist	275.43	2					34			X	
		END OF BOREHOLE NOTE: Upon completion of drilling:											

LGBE3 5555-21-GC.GPJ 4/28/21

NOTE: THE BOREHOLE DATA NEEDS INTERPRETATION ASSISTANCE BY TORONTO INSPECTION LTD. BEFORE USE BY OTHERS

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Time	Water Level (m)	Depth to Cave (m)



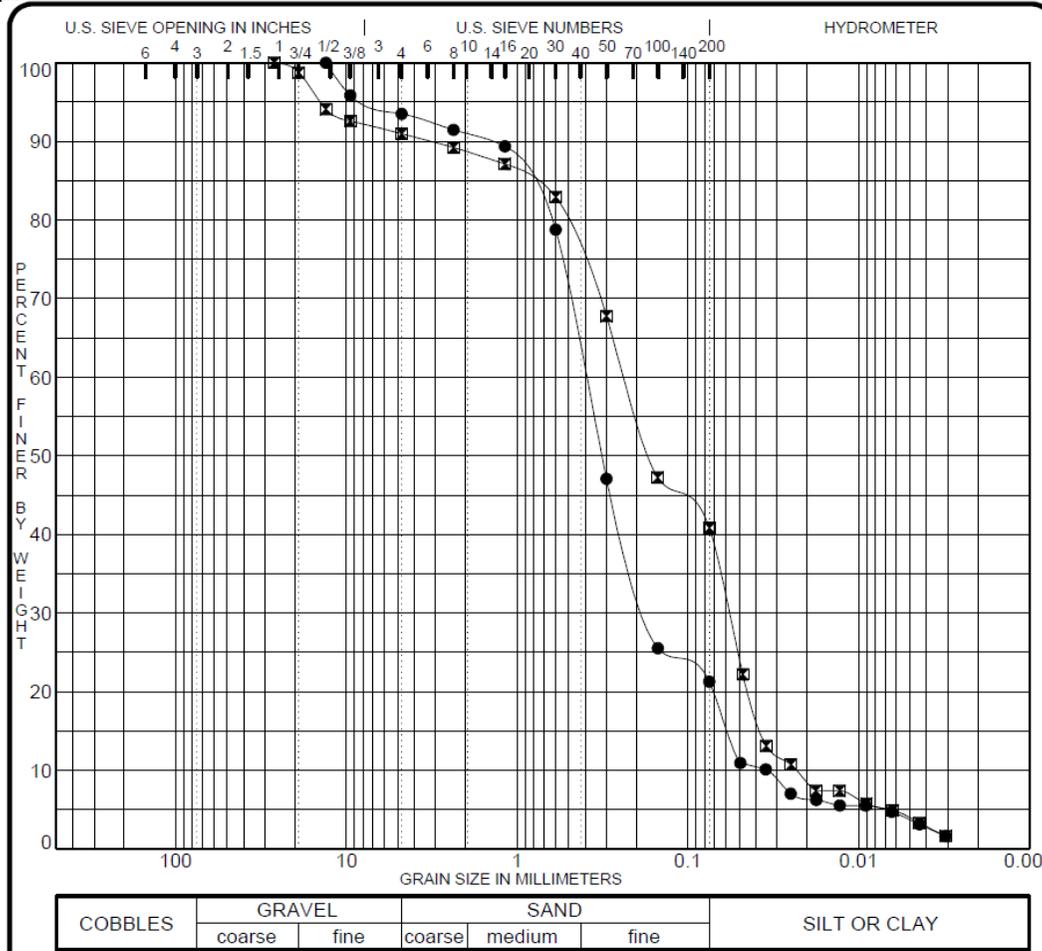
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APPENDIX B

Grain Size Analysis Gradation Curve

Grainsize Analyses: 23TP-2 1.41 mbgs

Company:	TIL
Client:	Man Holdings Ltd.
Project:	5555
Location:	181 Toronto Street South, Uxbridge, ON
Test Well:	23TP-2 1.41 mbgs
Test Date:	10-Jul-23
Test Conducted By:	KN





Toronto Inspection Ltd.

APPENDIX C

Infiltration Test Calculations and Guelph Permeameter Field Data

Input
 Result

Single Head Method (1)

Reservoir Cross-sectional area in cm^2
 (enter "35.22" for Combined and "2.16" for Inner reservoir): 35.22
 Enter water Head Height ("H" in cm): 5
 Enter the Borehole Radius ("a" in cm): 3

Enter the soil texture-structure category (enter one of the below numbers): 3

1. Compacted, Structure-less, clayey or silty materials such as landfill caps and liners, lacustrine or marine sediments, etc.
2. Soils which are both fine textured (clayey or silty) and unstructured; may also include some fine sands.
3. Most structured soils from clays through loams; also includes unstructured medium and fine sands. The category most frequently applicable for agricultural soils.
4. Coarse and gravelly sands; may also include some highly structured soils with large and/or numerous cracks, macropors, etc

Steady State Rate of Water Level Change ("R" in cm/min): 1.2000

Res Type 35.22
 H 5
 a 3
 H/a 1.667
 a* 0.12
 C0.01 0.809
 C0.04 0.842
 C0.12 0.803
 C0.36 0.803
 C 0.803
 R 1.200
 Q 0.704
 pi 3.142

$\alpha^* =$ 0.12 cm^{-2}
 C = 0.80315
 Q = 0.7044
 $K_{fs} =$ 1.28E-03 cm/sec
7.69E-02 cm/min
1.28E-05 m/sec
3.03E-02 $inch/min$
5.04E-04 $inch/sec$
 $\Phi_m =$ 1.07E-02 cm^2/min

Single Head Method (2)

Reservoir Cross-sectional area in cm^2
 (enter "35.22" for Combined and "2.16" for Inner reservoir): 35.22
 Enter water Head Height ("H" in cm): 10
 Enter the Borehole Radius ("a" in cm): 3

Enter the soil texture-structure category (enter one of the below numbers): 3

1. Compacted, Structure-less, clayey or silty materials such as landfill caps and liners, lacustrine or marine sediments, etc.
2. Soils which are both fine textured (clayey or silty) and unstructured; may also include some fine sands.
3. Most structured soils from clays through loams; also includes unstructured medium and fine sands. The category most frequently applicable for agricultural soils.
4. Coarse and gravelly sands; may also include some highly structured soils with large and/or numerous cracks, macropors, etc

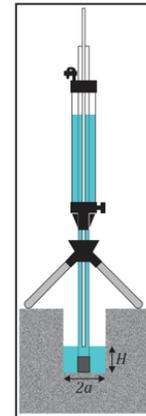
Steady State Rate of Water Level Change ("R" in cm/min): 1.6000

Res Type 35.22
 H 10
 a 3
 H/a 3.33333
 a* 0.12
 C0.01 1.21841
 C0.04 1.29023
 C0.12 1.28754
 C0.36 1.28754
 C 1.28754
 R 1.600
 Q 0.9392
 pi 3.1415

$\alpha^* =$ 0.12 cm^{-2}
 C = 1.28754
 Q = 0.9392
 $K_{fs} =$ 1.02E-03 cm/sec
6.11E-02 cm/min
1.02E-05 m/sec
2.40E-02 $inch/min$
4.01E-04 $inch/sec$
 $\Phi_m =$ 8.48E-03 cm^2/min

Average

$K_{fs} =$ 1.15E-03 cm/sec
6.90E-02 cm/min
1.15E-05 m/s
2.72E-02 $inch/min$
4.53E-04 $inch/sec$
 $\Phi_m =$ 9.58E-03 cm^2/min



Infiltration Test Calculation at 23TP-1 at 1.42 mbgs

Table 1: Guelph Permeameter Data at 23TP-1 at 1.42 mbgs

5 cm Head			10 cm Head		
Combined Reservoir			Combined Reservoir		
Time (min)	Reading (cm)	Rate (cm/min)	Time (min)	Reading (cm)	Rate (cm/min)
0	0		0	12.9	
1	4.9	4.9	1	20	7.1
2	6.2	1.3	4	22	2
3	7.8	1.5	6	23.8	1.8
4	9.0	1.2	8	25.8	2.0
5	10.2	1.2	9	27.4	1.6
6	11.4	1.2	10	29.5	1.5
7	12.6	1.2	11	31.2	1.7
			12	33.4	2.2
			13	35	1.6
			14	36.6	1.6
			15	38.2	1.6
			16	39.8	1.6

Input
 Result

Single Head Method (1)

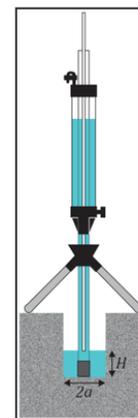
Reservoir Cross-sectional area in cm ² (enter "35.22" for Combined and "2.16" for Inner reservoir):	35.22
Enter water Head Height ("H" in cm):	5
Enter the Borehole Radius ("a" in cm):	3
Enter the soil texture-structure category (enter one of the below numbers): 3 	
<ol style="list-style-type: none"> 1. Compacted, Structure-less, clayey or silty materials such as landfill caps and liners, lacustrine or marine sediments, etc. 2. Soils which are both fine textured (clayey or silty) and unstructured; may also include some fine sands. 3. Most structured soils from clays through loams; also includes unstructured medium and fine sands. The category most frequently applicable for agricultural soils. 4. Coarse and gravely sands; may also include some highly structured soils with large and/or numerous cracks, macropors, etc 	
Steady State Rate of Water Level Change ("R" in cm/min): 0.3000 	
Res Type 35.22	
H 5	
a 3	$\alpha^* = $ 0.12 cm ⁻¹
H/a 1.667	C = 0.80315
a* 0.12	Q = 0.1761
C0.01 0.809	$K_{fs} = $ 3.20E-04 cm/sec
C0.04 0.842	 1.92E-02 cm/min
C0.12 0.803	 3.20E-06 m/sec
C0.36 0.803	 7.57E-03 inch/min
C 0.803	 1.26E-04 inch/sec
R 0.300	
Q 0.176	
pi 3.142	
	$\Phi_m = $ 2.67E-03 cm ² /min

Single Head Method (2)

Reservoir Cross-sectional area in cm ² (enter "35.22" for Combined and "2.16" for Inner reservoir):	35.22
Enter water Head Height ("H" in cm):	10
Enter the Borehole Radius ("a" in cm):	3
Enter the soil texture-structure category (enter one of the below numbers): 3 	
<ol style="list-style-type: none"> 1. Compacted, Structure-less, clayey or silty materials such as landfill caps and liners, lacustrine or marine sediments, etc. 2. Soils which are both fine textured (clayey or silty) and unstructured; may also include some fine sands. 3. Most structured soils from clays through loams; also includes unstructured medium and fine sands. The category most frequently applicable for agricultural soils. 4. Coarse and gravely sands; may also include some highly structured soils with large and/or numerous cracks, macropors, etc 	
Steady State Rate of Water Level Change ("R" in cm/min): 0.4000 	
Res Type 35.22	
H 10	
a 3	$\alpha^* = $ 0.12 cm ⁻¹
H/a 3.33333	C = 1.28754
a* 0.12	Q = 0.2348
C0.01 1.21841	$K_{fs} = $ 2.54E-04 cm/sec
C0.04 1.29023	 1.53E-02 cm/min
C0.12 1.28754	 2.54E-06 m/sec
C0.36 1.28754	 6.01E-03 inch/min
C 1.28754	 1.00E-04 inch/sec
R 0.400	
Q 0.2348	
pi 3.1415	
	$\Phi_m = $ 2.12E-03 cm ² /min

Average

$K_{fs} = $ 2.87E-04 cm/sec
 1.72E-02 cm/min
 2.87E-06 m/s
 6.79E-03 inch/min
 1.13E-04 inch/sec
$\Phi_m = $ 2.39E-03 cm ² /min



Infiltration Test Calculation at 23TP-2 at 1.41 mbgs

Table 2: Guelph Permeameter Data at 23TP-2 at 1.41 mbgs

5 cm Head			10 cm Head		
Combined Reservoir			Combined Reservoir		
Time (min)	Reading (cm)	Rate (cm/min)	Time (min)	Reading (cm)	Rate (cm/min)
0	0		0	3.5	
1	1.7	1.7	1	5.1	4.0
2	1.9	1.15	2	5.8	2.0
3	2.0	1.85	3	6.0	3.0
4	2.5	0.5	4	6.1	3.5
5	3.0	0.5	5	6.6	3.5
6	3.5	0.5	6	8.2	3.5
			7	10.0	1.8
			8	11.0	1.0
			9	12.0	1.0
			10	13.0	1.0